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(54) **Improved processability of silica filled rubber stocks**

Verbesserte Verarbeitbarkeit von Silica-gefüllten Kautschukzusammensetzungen

Mise en oeuvre améliorée de compositions de caoutchouc chargé en silice

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DE-A- 4 308 311 **US-A- 4 436 847**

EP 0 890 606 B1

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EP 0 890 606 B1

Description

TECHNICAL FIELD

5 [0001] The subject invention relates to the processing and vulcanization of diene polymer and copolymer elastomer containing rubber stocks. More specifically, the present invention relates to the processing and vulcanization of diene polymer and copolymer elastomer-containing, silica-filled rubber stocks using a mixture of silanes as processing aids.

BACKGROUND OF THE INVENTION

10 [0002] In the art it is desirable to produce elastomeric compounds exhibiting reduced hysteresis when properly compounded with other ingredients such as reinforcing agents, followed by vulcanization. Such elastomers, when compounded, fabricated and vulcanized into components for constructing articles such as tires, power belts, and the like, will manifest properties of increased rebound, decreased rolling resistance and less heat-build up when subjected to mechanical stress during normal use.

15 [0003] The hysteresis of an elastomer refers to the difference between the energy applied to deform an article made from the elastomer and the energy released as the elastomer returns to its initial, undeformed state. In pneumatic tires, lowered hysteresis properties are associated with reduced rolling resistance and heat build-up during operation of the tire. These properties, in turn, result in lowered fuel consumption of vehicles using such tires.

20 [0004] In such contexts, the property of lowered hysteresis of compounded, vulcanizable elastomer compositions is particularly significant. Examples of such compounded elastomer systems are known to the art and are comprised of at least one elastomer (that is, a natural or synthetic polymer exhibiting elastomeric properties, such as a rubber), a reinforcing filler agent (such as finely divided carbon black, thermal black, or mineral fillers such as clay and the like) and a vulcanizing system such as sulfur-containing vulcanizing (that is, curing) system.

25 [0005] Previous attempts at preparing readily processable, vulcanizable, silica-filled rubber stocks containing natural rubber or diene polymer and copolymer elastomers have focused upon the sequence of adding ingredients during mixing (*Bomal, et al., Influence of Mixing procedures on the Properties of a Silica Reinforced Agricultural Tire Tread; May 1992*), the addition of de-agglomeration agents such as zinc methacrylate and zinc octoate, or SBR-silica coupling agents such as mercapto propyl trimethoxy silane (*Hewitt, Processing Technology of Silica Reinforced SBR, Elastomerics, pp 33-37, March 1981*), and the use of bis[3-(triethoxysilyl)propyl]tetrasulfide (Si69) processing aid (*Degussa, PPG*).

30 [0006] The use of Si69 processing aid in the formulation of silica-filled rubber stocks has been successful, but generally requires a large amount of the additive, such as 10% by weight based on the weight of silica, in order to be effective.

35 [0007] Precipitated silica has been increasingly used as a reinforcing particulate filler in carbon black-filled rubber components of tires and mechanical goods. Silica-loaded rubber stocks, however, exhibit relatively poor processability.

40 [0008] US patent 4,436,847 describes a siliceous filler-reinforced rubber vulcanizate which is improved in abrasion resistance by adding to the unvulcanized rubber composition a silane coupling composition comprising a mixture of a silane coupling agent, such as (a) organic silane compounds containing an internal active olefinic linkage, (b) bis (alkoxysilylalkyl)polysulfides, (c) haloalkylsilanes, and (d) silane compounds containing a vinyl functional group in the organofunctional portion of the compound, and an alkyl alkoxysilane, such as methyltrimethoxysilane. The silane coupling agent is present in coupling amounts, e.g., between 0.1 and 50 parts per hundred parts of rubber, and the weight ratio of mercaptosilane to alkyl alkoxysilane is between 0.15:1 and 15:1. Preferably, the silanes are in a ratio of about 1:1, are admixed with a hydrocarbon process oil and the oil-silane mixture added to the siliceous filler-rubber mixture.

45 [0009] The present invention provides a mixture of silanes for use as processing aids for silica-filled rubber stocks, which greatly improve the processability and properties of the formulations and resulting vulcanized product.

SUMMARY OF INVENTION

50 [0010] It is therefore an object of the present invention to provide rubber stock processing aids which improve the processability of formulations of diene polymer elastomers with silica-filler.

[0011] It is another object of the present invention to provide a method for reducing the viscosity of silica-filled elastomeric vulcanizable compounds.

55 [0012] It is another object of the present invention to provide a method for enhancing the processability of silica-filled elastomeric vulcanizable compounds.

[0013] It is another object of the present invention to provide vulcanizable silica-filled elastomeric compounds having enhanced physical properties.

[0014] The foregoing objects, together with the advantages thereof over the existing art, which shall become apparent

EP 0 890 606 B1

from the specification which follows, are accomplished by the invention as hereinafter described and claimed.

[0015] The present invention provides a process for the preparation of a silica-filled, vulcanized elastomeric compound comprising effecting vulcanization of a mixture that comprises: (a) an elastomer; (b) a filler selected from the group consisting of amorphous silica and mixtures thereof with carbon black; (c) 0 to less than 1% by weight based on the weight of said silica of bis[3-(triethoxysilyl)propyl]tetrasulfide; (d) an alkyl- or arylalkoxysilane; (e) a processing aid comprising at least one of sorbitan esters of an oleate, laurate, palmate and stearate fatty acid and polyoxyethylene derivatives thereof; and (f) a cure agent. Preferably, the elastomer is a diene monomer homopolymer or a copolymer of a diene monomer and a monovinyl aromatic monomer.

[0016] The present invention further provides a silica-filled, vulcanized elastomeric compound obtainable by the above process of the invention.

[0017] Preferably, the elastomer is styrene butadiene rubber, optionally containing a carbon black filler. The compound is more readily processable during mixing, due to the use of the mixture of silane processing aids.

[0018] The present invention further provides a pneumatic tire comprising tread stock vulcanized from the inventive vulcanizable silica-filled compound.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0019] In general, the present invention provides a means to reduce the level of Si69 needed to obtain good physical properties in a cured rubber stock containing silica as a filler. In addition, the present invention further provides maintenance of the processability of the compounded stock, as measured by Mooney viscosity, at the same level as achieved with high levels of Si69.

[0020] The present invention utilizes the presence of an alkylalkoxysilane as a silica hydrophobating agent, such that minimal amounts of Si69 are needed to obtain good processability, and yet still give good physical properties. According to the invention, therefore, a less costly silane can be substituted for the majority or all of the Si69 that would be normally used without any loss of processability or properties. Additionally, remilling can be eliminated, and the cure of the rubber stock is not dependent on the high sulfur level present in the Si69.

[0021] The silica-hydrophobating agents useful according to the present invention include those alkyl- or arylalkoxysilanes of the formula $(R_1)_2Si(OR_2)_2$ or $R_1Si(OR_2)_3$, wherein the aryloxy or alkoxy groups are the same or are different; each R_1 independently comprising C1 to C18 aliphatic, C6 to C12 cyclo-aliphatic, or C6 to C18 aromatic, preferably C1 to C10 aliphatic, C6 to C10 cyclo-aliphatic, or C6 to C12 aromatic; and each R_2 independently containing from one to about 6 carbon atoms. Representative examples include octyltriethoxy silane, octyltrimethoxy silane, (3-glycidoxypropyl)triethoxy silane, (3-glycidoxypropyl)trimethoxy silane, hexyltriethoxy silane, ethyltriethoxy silane, ethyltrimethoxy silane, propyltriethoxy silane, phenyltriethoxy silane, cyclohexyltriethoxy silane, cyclohexyltriethoxy silane, dimethyldimethoxy silane, 3-chloropropyltriethoxy silane, methacryoltriethoxy silane, i-butyltriethoxy silane. Of these, octyltriethoxysilane is preferred.

[0022] According to the present invention, polymerized elastomer is compounded in the rubber stock, e.g., polybutadiene, polyisoprene and the like, and copolymers thereof with monovinyl aromatics such as styrene, alpha methyl styrene and the like, or trienes such as myrcene. Thus, the elastomers include diene homopolymers, A, and copolymers thereof with monovinyl aromatic polymers, B. Exemplary diene homopolymers are those prepared from diolefin monomers having from 4 to 12 carbon atoms. Exemplary vinyl aromatic polymers are those prepared from monomers having from 8 to 20 carbon atoms. Examples of conjugated diene monomers and the like useful in the present invention include 1,3-butadiene, isoprene, 1,3-pentadiene, 2,3-dimethyl-1,3-butadiene and 1,3-hexadiene, and aromatic vinyl monomers include styrene, α -methylstyrene, p-methylstyrene, vinyltoluenes and vinylnaphthalenes. The conjugated diene monomer and aromatic vinyl monomer are normally used at the weight ratios of 90:10 to 55:45, preferably 80:20 to 65:35.

[0023] Preferred elastomers include diene homopolymers such as polybutadiene and polyisoprene and copolymers such as styrene butadiene rubber (SBR). Copolymers can comprise from 99 to 20 percent by weight of diene units and from 1 to 80 percent by weight of monovinyl aromatic or triene units, totaling 100 percent. The polymers and copolymers of the present invention may have the diene portion with a 1,2-microstructure contents ranging from 10 to 80 percent, with the preferred polymers or copolymers having 1,2-microstructure contents of from 125 to 65 percent. The molecular weight of the polymer that is produced according to the present invention, is preferably such that a proton-quenched sample will exhibit a gum Mooney viscosity ($ML_4/212^\circ F$) of from about 2 to 150. The copolymers are preferably random copolymers which result from simultaneous copolymerization of the monomers, as is known in the art. Also included are nonfunctionalized cis-polybutadiene, ethylene-propylene-diene monomer (EPDM), emulsion SBR and natural rubber.

[0024] Initiators known in the art such as an organolithium initiator, preferably an alkylolithium initiator, can be employed to prepare the elastomer. More particularly, the initiators used in the present invention include N-lithio-hexamethylenimine, organolithium compounds such as n-butyllithium, tributyltin lithium, dialkylaminolithium compounds such as

EP 0 890 606 B1

dimethylaminolithium, diethylaminolithium, dipropylaminolithium, dibutylaminolithium and the like, dialkylaminoalkyl-lithium compounds such as diethylaminopropylolithium and the like, and trialkyl stanyl lithium, wherein the alkyl group contains 1 to 12 carbon atoms, preferably 1 to 4 carbon atoms.

[0025] Polymerization is usually conducted in a conventional solvent for anionic polymerizations such as the various cyclic and acyclic hexanes, heptanes, octanes, pentanes, their alkylated derivatives, and mixtures thereof. Other techniques for polymerization, such as semi-batch and continuous polymerization may be employed. In order to promote randomization in copolymerization and to increase vinyl content, a coordinator may optionally be added to the polymerization ingredients. Amounts range between 0 to 90 or more equivalents per equivalent of lithium. The amount depends upon the amount of vinyl desired, the level of styrene employed and the temperature of the polymerizations, as well as the nature of the specific polar coordinator employed.

[0026] Compounds useful as coordinators are organic and include those having an oxygen or nitrogen hetero-atom and a non-bonded pair of electrons. Examples include dialkyl ethers of mono and oligo alkylene glycols; "crown" ethers; tertiary amines such as tetramethylethylene diamine (TMEDA); THF; THF oligomers; linear and cyclic oligomeric oxolanyl alkanes, such as 2-2'-di(tetrahydrofuryl) propane, di-piperidyl ethane, hexamethylphosphoramide, N-N'-dimethylpiperazine, diazabicyclooctane, diethyl ether, tributylamine and the like. Details of linear and cyclic oligomeric oxolanyl coordinators can be found in U.S. Pat. No. 4,429,091, owned by the Assignee of record.

[0027] Polymerization is usually begun by charging a blend of the monomer(s) and solvent to a suitable reaction vessel, followed by the addition of the coordinator and the initiator solution previously described. Alternatively, the monomer and coordinator can be added to the initiator. The procedure is carried out under anhydrous, anaerobic conditions. The reactants are heated to a temperature of from 10° to 150°C and are agitated for 0.1 to 24 hours. After polymerization is complete, the product is removed from the heat and terminated in one or more ways.

[0028] To terminate the polymerization, a terminating agent, coupling agent or linking agent may be employed, all of these agents being collectively referred to herein as "terminating agents". Certain of these agents may provide the resulting polymer with a multifunctionality. That is, the polymers initiated according to the present invention, carry at least one amine functional group as discussed hereinabove, and may also carry a second functional group selected and derived from the group consisting of terminating agents, coupling agents and linking agents.

[0029] Examples of terminating agents according to the present invention include those commonly employed in the art, including hydrogen, water, steam, an alcohol such as isopropanol, 1,3-dimethyl-2-imidazolidinone (DMI), carbodiimides, N-methylpyrrolidine, cyclic amides, cyclic ureas, isocyanates, Schiff bases, 4,4'-bis(diethylamino) benzophenone, and the like. Other useful terminating agents may include those of the structural formula $(R_1)_a ZX_b$, wherein Z is tin or silicon. It is preferred that Z is tin. R_1 is an alkyl having from 1 to 20 carbon atoms; a cycloalkyl having from 3 to 20 carbon atoms; an aryl having from 6 to 20 carbon atoms; or, an aralkyl having from 7 to 20 carbon atoms. For example, R_1 may include methyl, ethyl, n-butyl, neophyl, phenyl, cyclohexyl or the like. X is a halogen, such as chlorine or bromine, or an alkoxy ($-OR_1$), "a" is from 0 to 3, and "b" is from 1 to 4; where $a + b = 4$. Examples of such terminating agents include tin tetrachloride, $(R_1)_3SnCl$, $(R_1)_2SnCl_2$, R_1SnCl_3 , and R_1SiCl_3 as well as methyltriphenoxysilane ($MeSi(OPh_3)$).

[0030] The terminating agent is added to the reaction vessel, and the vessel is agitated for 1 to about 1000 minutes. As a result, an elastomer is produced having an even greater affinity for silica compounding materials, and hence, even further reduced hysteresis. Additional examples of terminating agents include those found in U.S. Patent No. 4,616,069. It is to be understood that practice of the present invention is not limited solely to these terminators inasmuch as other compounds that are reactive with the polymer bound lithium moiety can be selected to provide a desired functional group.

[0031] Quenching is usually conducted by stirring the polymer and quenching agent for 0.05 to 2 hours at temperatures of from 30° to 120° C to ensure complete reaction. Polymers terminated with a functional group as discussed hereinabove, can be subsequently quenched with alcohol or other quenching agents as described hereinabove.

[0032] Lastly, the solvent is removed from the polymer by conventional techniques such as drum drying, extruder drying, vacuum drying or the like, which may be combined with coagulation with water, alcohol or steam, thermal desolventization, or any other suitable method. If coagulation with water or steam is used, oven drying may be desirable.

[0033] The elastomeric polymers can be utilized as 100 parts of the rubber in the treadstock compound or, they can be blended with any conventionally employed treadstock rubber which includes natural rubber, synthetic rubber and blends thereof. Such rubbers are well known to those skilled in the art and include synthetic polyisoprene rubber, styrene/butadiene rubber (SBR), polybutadiene, butyl rubber, Neoprene, ethylene/propylene rubber, ethylene/propylene/diene rubber (EPDM), acrylonitrile/butadiene rubber (NBR), silicone rubber, the fluoroelastomers, ethylene acrylic rubber, ethylene vinyl acetate copolymer (EVA), epichlorohydrin rubbers, chlorinated polyethylene rubbers, chlorosulfonated polyethylene rubbers, hydrogenated nitrile rubber, tetrafluoroethylene/propylene rubber and the like. When the polymers discussed hereinabove are blended with conventional rubbers, the amounts can vary widely with a range comprising 5 to 99 percent by weight of the total rubber. It is to be appreciated that the minimum amount will depend primarily upon the degree of reduced hysteresis that is desired.

EP 0 890 606 B1

[0034] According to the present invention, amorphous silica (silicon dioxide) is utilized as a filler for the diene polymer or copolymer elastomer-containing vulcanizable compound. Silicas are generally classed as wet-process, hydrated silicas because they are produced by a chemical reaction in water, from which they are precipitated as ultrafine, spherical particles.

[0035] These primary particles strongly associate into aggregates, which in turn combine less strongly into agglomerates. The surface area, as measured by the BET method gives the best measure of the reinforcing character of different silicas. For silicas of interest for the present invention, the surface area should be 32 to 400 m²/g, with the range of 100 to 250 m²/g being preferred, and the range of 150 to 220 m²/g being most preferred. The pH of the silica filler is generally 5.5 to 7 or slightly over, preferably 5.5 to 6.8.

[0036] Silica can be employed in the amount of 1 part to 100 parts per 100 parts of polymer (phr), preferably in an amount from 5 to 80 phr. The useful upper range is limited by the high viscosity imparted by fillers of this type. Some of the commercially available silicas which may be used include: Hi-Sil® 215, Hi-Sil® 233, and Hi-Sil® 190, all produced by PPG Industries. Also, a number of useful commercial grades of different silicas are available from De Gussa Corporation, Rhone Poulenc, and J.M. Huber Corporation.

[0037] The polymers can be compounded with all forms of carbon black in amounts ranging from 2 to 50 parts by weight, per 100 parts of rubber (phr), with 5 to 40 phr being preferred. The carbon blacks may include any of the commonly available, commercially-produced carbon blacks but those having a surface area (EMSA) of at least 20 m²/gram and more preferably at least 35 m²/gram up to 200 m²/gram or higher are preferred. Surface area values used in this application are those determined by ASTM test D-1765 using the cetyltrimethyl-ammonium bromide (CTAB) technique. Among the useful carbon blacks are furnace black, channel blacks and lamp blacks. More specifically, examples of the carbon blacks include super abrasion furnace (SAF) blacks, high abrasion furnace (HAF) blacks, fast extrusion furnace (FEF) blacks, fine furnace (FF) blacks, intermediate super abrasion furnace (ISAF) blacks, semi-reinforcing furnace (SRF) blacks, medium processing channel blacks, hard processing channel blacks and conducting channel blacks. Other carbon blacks which may be utilized include acetylene blacks. Mixtures of two or more of the above blacks can be used in preparing the carbon black products of the invention. Typical values for surface areas of usable carbon blacks are summarized in the Table I hereinbelow.

TABLE I

Carbon Blacks	
ASTM Designation (D-1765-82a)	Surface Area (m ² /g) (D-3765)
N-110	126
N-220	111
N-339	95
N-330	83
N-351	74
N-550	42
N-660	35

[0038] The carbon blacks utilized in the preparation of the rubber compounds of the invention may be in pelletized form or an unpelletized flocculent mass. Preferably, for more uniform mixing, unpelletized carbon black is preferred.

[0039] The reinforced rubber compounds can be cured in a conventional manner with known vulcanizing agents at 0.2 to 5 phr. For example, sulfur or peroxide-based curing systems may be employed. For a general disclosure of suitable vulcanizing agents one can refer to Kirk-Othmer, Encyclopedia of Chemical Technology, 3rd ed., Wiley Interscience, N.Y. 1982, Vol. 20, pp. 365-468, particularly "Vulcanization Agents and Auxiliary Materials" pp. 390-402. Vulcanizing agents can be used alone or in combination.

[0040] Vulcanizable elastomeric compositions of the invention can be prepared by compounding or mixing the elastomeric polymer with silica, optionally carbon black, the silica-hydrophobating agent according to the present invention, a minimal amount of Si69, and other conventional rubber additives including for example, fillers, plasticizers, antioxidants, curing agents and the like, using standard rubber mixing equipment and procedures.

GENERAL EXPERIMENTAL

[0041] In order to demonstrate the preparation and properties of silica-filled, diene elastomer containing rubber stocks prepared according to the present invention, styrene butadiene rubber (SBR) polymers were prepared and were compounded using the formulations set forth in Tables II and III below.

EP 0 890 606 B1

[0042] Test results for the Control, C-A, using the Si69 processing aid only, and Examples 1 - 3, using silane processing aids according to the invention in Formulation A, are reported in Table II.

TABLE II

Formulation A for the Partial Replacement of Si69 and Physical Test Results				
Material	Amount (phr)			
Example No.	C-A	1	2	3
SBR	100	100	100	100
Oil	20	20	20	20
Silica	60	60	60	60
Carbon Black	6	6	6	6
Stearic Acid	2	2	2	2
Wax	0.75	0.75	0.75	0.75
Si-69	5.4	0.6	0.6	0.6
Silane (Type)	--	Octyl Trimethoxy	Methacroyl Trimethoxy	Dimethyl Dimethoxy
Silane (Amount)	0	4.71	4.99	3.62
Tackifier	3.5	3.5	3.5	3.5
Antioxidant	0.95	0.95	0.95	0.95
Sulfur	1.4	1.4	1.4	1.4
Accelerators	2.4	2.4	2.4	2.4
Zinc Oxide	3	3	3	3
Physical Properties				
ML ₁₊₄ @ 100°C	93.7	84.7	93.3	88.8
Tensile (psi) @ 23°C (a)	2913	2216	2476	2834
Tensile (psi) @ 100°C (a)	1239	954	1122	1294
% Elong. at break, 23°C	444	603	504	551
% Elong. at break, 100°C	262	407	342	365
Ring Tear (lb/in) @ 100°C (b)	191	198	179	223
Dispersion Index, %	72.9	76.1	84	84.3

(a) Values given in psi can be converted to the corresponding values in kPa by multiplication by 6.896.

(b) Values given in lb/in can be converted to the corresponding values in kg/m by multiplication by 17.858.

[0043] Test results for the Control, C-B, using the Si69 processing aid only, and Examples 4 - 7, using silane processing aids according to the invention in Formulation B, are reported in Table III.

TABLE III

Formulation B for the Partial Replacement of Si69 and Physical Test Results					
Material	Amount (phr)				
Example No.	C-B	4	5	6	7
SBR	75	75	75	75	75
BR	25	25	25	25	25
Oil	41.25	41.25	41.25	41.25	41.25
Silica	80	80	80	80	80
Carbon Black	8	8	8	8	8
Stearic Acid	1	1	1	1	1
Wax	1.5	1.5	1.5	1.5	1.5
Si-69	7.2	0.8	0.8	0.8	0.8
Silane (Type)	--	Propyl Triethoxy	3-Chloropropyl Triethoxy	Octyl Triethoxy	i-Butyl Triethoxy
Silane (Amount)	0	5.5	6.42	7.39	5.88

EP 0 890 606 B1

TABLE III (continued)

Formulation B for the Partial Replacement of Si69 and Physical Test Results					
Material	Amount (phr)				
Example No.	C-B	4	5	6	7
Tackifier	3	3	3	3	3
Antioxidant	1.17	1.17	1.17	1.17	1.17
Sulfur	2.8	2.8	2.8	2.8	2.8
Accelerators	2.4	2.4	2.4	2.4	2.4
Zinc Oxide	1.7	1.7	1.7	1.7	1.7
Physical Properties					
ML ₁₊₄ @ 100°C	64.8	69.2	96.1	53.8	93.9
Tensile (psi) @ (a) 23°C	2497	2268	2566	2400	2513
Tensile (psi) @ (a) 100°C	1453	1278	1693	1280	1379
% Elong. at break, 23°C	487	614	544	612	649
% Elong. at break, 100°C	386	486	487	467	499
Ring Tear (lb/in) @ (b) 100°C	190	270	245	262	298
Dispersion Index, %	93.1	80.5	95.7	87.9	93.3

(a) Values given in psi can be converted to the corresponding values in kPa by multiplication by 6.896.

(b) Values given in lb/in can be converted to the corresponding values in kg/m by multiplication by 17.858.

[0044] A series of tests were conducted, in which the Si69 processing aid was omitted and insoluble sulfur was added, while processing Formulation B with 2 phr octyl-triethoxy silane, and 4 phr sorbitan oleate. Test conditions and results are reported for Examples 8 -17 and the Control (no added insoluble sulfur), C-C, in Table IV, below.

EP 0 890 606 B1

TABLE IV
Physical Properties of Formulation B with 2 phr Octyl-Triethoxy Silane, 4 phr Sorbitan Monooleate, and Insoluble Sulfur without Si69

Sample	8	9	10	11	12	13	14	15	16	17	C-C
Insoluble S (phr)	1.4	1.7	2	2.3	2.6	2.9	3.3	3.7	4.1	4.5	0
Total S (phr)	2.8	3.1	3.4	3.7	4	4.3	4.7	5.1	5.5	5.9	1.4
Physical Test Results											
ML ₁₊₄ /100°C	84	81.9	80.7	78.9	78.5	103.6	101.8	99.5	99.8	101.7	75.7
Monsanto Cure @ 171°C											
ML	13.6	14.7	13.4	13	12.8	18	18.2	18	17.8	18.2	116
MH	33.4	34.8	37.1	37	38.3	46.5	48.3	50.6	50.8	53.9	37.37
ts2	2:54	2:48	2:41	2:47	2:44	2:42	2:34	2:30	2:28	2:29	2:30
tc90	10:51	9:50	9:42	9:28	9:15	12:05	11:36	11:11	10:29	11:11	10:01
Ring Tensile @ 24°C											
100% Modulus, psi (a)	188	184	209	194	227	212	267	256	284	326	318
300% Modulus, psi (a)	494	485	592	556	667	670	792	765	872	988	1150
Tensile str, psi (a)	1798	1550	1814	1548	1769	1842	2120	1757	1925	2076	2809
% Elongation	724	657	641	613	594	601	591	538	527	510	556
Break energy, lbs/in ² (b)	5273	4203	4835	4000	4445	4569	5196	4034	4343	4580	6596

EP 0 890 606 B1

TABLE IV CONTINUED

Sample	8	9	10	11	12	13	14	15	16	17	C
Ring Tensile @ 100°C											
100% Modulus, psi (a)	131	151	191	215	187	210	231	255	286	292	268
300% Modulus, psi (a)	333	381	519	566	532	621	656	730	846	833	661
Tensile str, psi (a)	905	1062	1233	1162	983	1156	1017	878	1079	1042	1263
% Elongation	649	652	592	529	500	500	441	340	375	364	364
Break Energy, lbs/in ² (b)	2612	3070	3306	2850	2310	2849	2172	1565	1984	1906	2092
Ring Tear @ 171°C, ppi (c)	250	217	228	230	201	247	216	201	192	221	276
Pendulum Rebound 65°C	33.6	35	32.4	37.6	40.2	37.2	40.2	37.6	41.2	41.4	53.6
Wet Stanley London, (#/std)	56/53	54/53	56/53	53/53	57/53	60/54	62/54	63/54	64/54	63/54	
Shore A @ 24°C	68	67	68	68	69	71	71	73	73	72	65
Dispersion Index #1	85.6	85.5	86.5	87.1	88						59.4
Specific Gravity	1.184	1.186	1.189	1.188	1.189	1.195	1.197	1.199	1.199	1.21	1.202
Rheometries @ 7% strain											
tan δ @ 65°C	.1978	.1924	.1807	.1858	.1789	.1697	.1662	.158	.1583	.1503	.1839
$\Delta G'$ @ 65°C, MPa	4.884	6.201	6.133	5.937	6.117	7.747	8.845	9.295	9.552	10.041	6.88
Tensile Retraction											
Mc x 10 ⁻³ g/mol	20.9	20.0	17.5	17.4	16.3	15.4			13.2	12.3	12.2

(a) Values given in psi can be converted to the corresponding values in kPa by multiplication by 6.896.

(b) Values given in lbs/in² can be converted to the corresponding values in kg/m² by multiplication by 703.1.

(c) Values given in ppi (lb/in) can be converted to the corresponding values in kg/m by multiplication by 17.858.

EP 0 890 606 B1

[0045] A further series of tests were conducted, in which Formulation B, described in Table III, was processed with added sulfur and a processing aid comprising 1.5 phr octyl-triethoxy silane, 0.5 phr Si69, and 4 phr sorbitan oleate. Test conditions and results are reported for Examples 18 - 22 in Table V, below.

TABLE V

Physical Properties of Formulation B with 1.5 phr Octyl-triethoxysilane, 4 phr Sorbitan, 0.5 Si69 and Insoluble Sulfur					
Sample	18	19	20	21	22
Insoluble S (phr)	2.8	3.2	3.6	4	4.4
Total S (phr)	4.2	4.6	5	5.4	5.8
Physical Test Results					
ML ₁₊₄ /100°C	81.9	83.6	84.2	86.3	80.8
Monsanto Cure @ 171°C					
ML	13.15	13.2	13.15	13.82	12.48
MH	41.84	44.62	44.62	46.58	46.98
ts2	2:50	2:44	2:43	2:35	2:38
tc90	10:15	10:12	9:12	9:24	8:59
Ring Tensile @ 24°C					
100 % Modulus, psi (a)	273	291	326	341	408
300 % Modulus, psi (a)	935	994	1112	1158	1452
Tensile str, psi (a)	2323	2183	2112	2012	2497
% Elongation	582	537	483	461	460
Break Energy, lbs/in ² (b)	5760	5099	4545	4164	5130
Ring Tensile @ 100°C					
100 % Modulus, psi (a)	251	251	287	307	311
300 % Modulus, psi (a)	826	798	933	1030	998
Tensile str, psi (a)	1326	1215	1255	1229	1113
% Elongation	444	428	388	350	329
Break Energy, lbs/in ² (b)	2720	2439	2306	2069	1800
Ring Tear @ 171°C, psi (a)	240	230	201	219	206
Pendulum Rebound 65°C	37.2	39	42.8	39.4	42.4
Wet Stanley London (#/std)	64/53	61/53	64/53	65/53	65/53
Shore A, @ RT	72	71	72	74	73
Specific Gravity	1.195	1.196	1.197	1.197	1.202
Rheometries @ 7 % strain					
tan δ @ 65°C	0.1577	0.1528	0.1444	0.1384	0.1533
Δ G' @ 65°C, MPa	6.89	6.798	6.676	6.285	7.789
Tensile Retraction Mc, x 10 ⁻³ g/mol	12.6	12.4	11.1	10.4	9.7

(a) Values given in psi can be converted to the corresponding values in kPa by multiplication by 6.896.

(b) Values given in lbs/in² can be converted to the corresponding values in kg/m² by multiplication by 703.1.

[0046] The present invention can thus further utilize the presence of an ester of a fatty acid or an ester of a polyol as a processing aid to replace the silane Si69 to give equal processability of the vulcanizable compound, and better hot tear strength and lower hysteresis of the vulcanized rubber stock, without loss of the other measured physical properties.

[0047] The further processing aid, such as the preferred sorbitan oleate, is air stable and does not decompose. The sorbitan oleate is lower in cost and more storage stable than Si69, and when used with a silica filler and a silane terminated polymer, gives similar reduction of ML₄, and tan δ with an increase in tear strength.

[0048] The additional processing aids useful according to the present invention include esters of fatty acids or esters of polyols. Representative examples include the sorbitan oleates, such as sorbitan monooleate, dioleate, trioleate and sesquioleate, as well as sorbitan esters of laurate, palmate and stearate fatty acids, and the polyoxyethylene derivatives

EP 0 890 606 B1

of each, and other polyols, including glycols such as polyhydroxy compounds and the like. Of these, sorbitan monooleate is preferred.

[0049] It is therefore demonstrated that the present invention provides a means for improving the processability of formulations of diene polymer elastomers with silica-filler, reducing the viscosity of silica-filled elastomeric vulcanizable compounds. It is further demonstrated that the present invention provides vulcanizable silica-filled elastomeric compounds having enhanced physical properties.

[0050] It should be appreciated that the present invention is not limited to the specific embodiments described above, but includes variations, modifications and equivalent embodiments defined by the following claims.

Claims

1. A process for the preparation of a silica-filled, vulcanized elastomeric compound comprising effecting vulcanization of a mixture that comprises:

- (a) an elastomer;
- (b) a filler-selected from the group consisting of amorphous silica and mixtures thereof with carbon black;
- (c) 0 to less than 1% by weight based on the weight of said silica of bis[3-(triethoxysilyl)propyl]tetrasulfide;
- (d) an alkyl- or arylalkoxysilane;
- (e) a processing aid comprising at least one of sorbitan esters of an oleate, laurate, palmate and stearate fatty acid and polyoxyethylene derivatives thereof; and
- (f) a cure agent.

2. The process as in claim 1 wherein the elastomer is a diene monomer homopolymer or a copolymer of a diene monomer and a monomer selected from the group consisting of monovinyl aromatic monomers and triene monomers.

3. The process as in claim 1 wherein the alkyl- or arylalkoxysilane is represented by the formula $(R_1)_2Si(OR_2)_2$ or $R_1Si(OR_2)_3$, wherein each R_1 independently is selected from the group consisting of C1 to C18 aliphatic, C6 to C12 cycloaliphatic, and C6 to C18 aromatic; and, wherein the alkoxy groups are the same or are different, each R_2 independently containing from one to 6 carbon atoms.

4. The process of claim 3 wherein the alkyl- or arylalkoxysilane comprises at least one of octyltriethoxy silane, octyltrimethoxy silane, hexyltrimethoxy silane, ethyltrimethoxy silane, propyltriethoxy silane, phenyltrimethoxy silane, cyclohexyltrimethoxy silane, cyclohexyltriethoxy silane, dimethyldimethoxy silane and i-butyltriethoxy silane.

5. The process of claim 1 wherein the processing aid comprises at least one of sorbitan monooleate, sorbitan dioleate, sorbitan trioleate and sorbitan sesquioleate.

6. The process of claim 1 wherein the elastomer contains a functional group derived from a polymerization initiator.

7. The process of claim 1, wherein the elastomer contains a functional group derived from a polymerization terminating agent and wherein the terminating agent is water, steam, an alcohol, 1,3-dimethyl-2-imidazolidinone, a carbodiimide, N-methylpyrrolidine, a cyclic amide, a cyclic urea, an isocyanate, a Schiff base, 4,4'-bis(diethylamino) benzophenone or an agent having the formula $(R_1)_aZX_b$, wherein Z is tin or silicon, R_1 is an alkyl having from 1 to 20 carbon atoms; a cycloalkyl having from 3 to 20 carbon atoms; an aryl having from 6 to 20 carbon atoms; or an aralkyl having from 7 to 20 atoms; X is a halogen or an alkoxy group; a is from 0 to 3, and b is from 1 to 4, and the sum of $a+b=4$.

8. The process of claim 1 wherein the mixture comprises insoluble sulfur.

EP 0 890 606 B1

9. A silica-filled, vulcanized elastomeric compound obtainable by the process according to any one of claims 1 to 8.
10. A pneumatic tire comprising tread stock vulcanized from the compound of claim 9.

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Patentansprüche

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1. Verfahren zur Herstellung einer Silica-gefüllten vulkanisierten elastomeren Masse, das die Vulkanisierung eines Gemisches umfasst, umfassend:

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- (a) ein Elastomer,
- (b) einen Füllstoff ausgewählt aus der Gruppe bestehend aus amorphen Silica und Gemischen davon mit Ruß,
- (c) 0 bis weniger als 1 Gew.-% bis[3-(triethoxysilyl)propyl]tetrasulfid, bezogen auf das Silicagewicht,
- (d) ein Alkyl- oder Arylalkoxysilan,
- (e) ein Verarbeitungshilfsmittel, umfassend mindestens eine Verbindung ausgewählt aus Sorbitanestern der Öl-, Laurin-, Palmitin- und Stearinfettsäure und Polyoxyethylenderivaten davon, und
- (f) ein Härtungsmittel.

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2. Verfahren nach Anspruch 1, wobei das Elastomer ein Homopolymer eines Dienmonomeren oder ein Copolymer eines Dienmonomeren und eines Monomeren, ausgewählt aus der Gruppe bestehend aus monovinylaromatischen Monomeren und Trienmonomeren, ist.

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3. Verfahren nach Anspruch 1, wobei das Alkyl- oder Arylalkoxysilan die allgemeine Formel $(R_1)_2Si(OR_2)_2$ oder $R_1Si(OR_2)_3$ aufweist, in der jeder der Reste R_1 unabhängig voneinander, ausgewählt ist aus der Gruppe bestehend aus C_1 - C_{18} aliphatischen Resten, C_6 - C_{12} cycloaliphatischen Resten und C_6 - C_{18} aromatischen Resten, und in der die Alkoxyreste gleich oder verschieden voneinander sind und jeder der Reste R_2 unabhängig voneinander 1 bis 6 Kohlenstoffatome enthält.

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4. Verfahren nach Anspruch 3, wobei das Alkyl- oder Arylalkoxysilan mindestens eine Verbindung umfasst, ausgewählt aus Octyltriethoxysilan, Octyltrimethoxysilan, Hexyltrimethoxysilan, Ethyltrimethoxysilan, Propyltriethoxysilan, Phenyltrimethoxysilan, Cyclohexyltrimethoxysilan, Cyclohexyltriethoxysilan, Dimethyldimethoxysilan und i-Butyltriethoxysilan.

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5. Verfahren nach Anspruch 1, wobei das Verarbeitungshilfsmittel mindestens eine Verbindung umfasst, ausgewählt aus Sorbitanmonooleat, Sorbitandioleat, Sorbitantrioleat und Sorbitanesesquioleat.

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6. Verfahren nach Anspruch 1, wobei das Elastomer eine von einem Polymerisationsinitiator abgeleitete funktionelle Gruppe enthält.

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7. Verfahren nach Anspruch 1, wobei das Elastomer eine von einem Polymerisationsabbruchmittel abgeleitete funktionelle Gruppe enthält und wobei das Abbruchmittel Wasser, Dampf, ein Alkohol, 1,3-Dimethyl-2-imidazolidinon, ein Carbodiimid, N-Methylpyrrolidin, ein zyklisches Amid, ein zyklischer Harnstoff, ein Isocyanat, eine Schiffsche Base, 4,4'-Bis(diethylamino) benzophenon oder ein Mittel mit der allgemeinen Formel $(R_1)_a ZX_b$, ist, in der Z Zinn oder Silicium ist, R_1 ein Alkylrest mit 1 bis 20 Kohlenstoffatomen, ein Cycloalkylrest mit 3 bis 20 Kohlenstoffatomen, ein Arylrest mit 6 bis 20 Kohlenstoffatomen oder ein Aralkylrest mit 7 bis 20 Kohlenstoffatomen ist, X ein Halogenatom oder ein Alkoxyrest ist, a gleich 0 bis 3, b gleich 1 bis 4 und die Summe aus $a+b=4$ ist.

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8. Verfahren nach Anspruch 1, wobei das Gemisch unlöslichen Schwefel umfasst.

9. Silicagefüllte, vulkanisierte elastomere Masse, erhältlich nach dem Verfahren gemäß einem der Ansprüche 1 bis 8.

10. Luftreifen, umfassend eine Laufflächenzusammensetzung vulkanisiert aus der Masse gemäß Anspruch 9.

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Revendications

1. Procédé pour la préparation d'un composé élastomère vulcanisé, additionné d'une charge consistant en silice, comprenant l'étape consistant à effectuer la vulcanisation d'un mélange qui comprend :

EP 0 890 606 B1

- (a) un élastomère ;
 (b) une charge choisie dans le groupe consistant en la silice amorphe et des mélanges de silice amorphe avec le noir de carbone ;
 (c) 0 à moins de 1 % en poids, sur la base du poids de ladite silice, de tétrasulfure de bis-[3-(triéthoxysilyl)propyle] ;
 (d) un alkyl- ou arylalkoxysilane ;
 (e) un adjuvant de traitement comprenant au moins un des esters de sorbitanne consistant en oléates, laurates, palmitates et stéarates d'acides gras et leurs dérivés formés avec le polyoxyéthylène ; et
 (f) un durcisseur.
2. Procédé suivant la revendication 1, dans lequel l'élastomère est un homopolymère de monomère diénique ou un copolymère d'un monomère diénique et d'un monomère choisi dans le groupe consistant en des monomères aromatiques monovinylés et des monomères consistant en triènes.
3. Procédé suivant la revendication 1, dans lequel l'alkyl- ou arylalkoxysilane est représenté par la formule $(R_1)_2Si(OR_2)_2$ ou $R_1Si(OR_2)_3$, dans laquelle chaque groupe R_1 est choisi indépendamment dans le groupe consistant en des groupes aliphatiques en C_1 à C_{18} , des groupes cycloaliphatiques en C_6 à C_{12} et des groupes aromatiques en C_6 à C_{18} ; et les groupes alkoxy sont identiques ou différents, chaque groupe R_2 contenant indépendamment 1 à 6 atomes de carbone.
4. Procédé suivant la revendication 3, dans lequel l'alkyl- ou arylalkoxysilane comprend au moins un des composés consistant en octyltriéthoxysilane, octyltriméthoxysilane, hexyltriméthoxysilane, éthyltriméthoxysilane, propyltriéthoxysilane, phényltriméthoxysilane, cyclohexyltriméthoxysilane, cyclohexyltriéthoxysilane, diméthyltriméthoxysilane et isobutyltriéthoxysilane.
5. Procédé suivant la revendication 1, dans lequel l'adjuvant de traitement comprend au moins un des composés consistant en mono-oléate de sorbitanne, dioléate de sorbitanne, trioléate de sorbitanne et sesquioléate de sorbitanne.
6. Procédé suivant la revendication 1, dans lequel l'élastomère contient un groupe fonctionnel dérivé d'un initiateur de polymérisation.
7. Procédé suivant la revendication 1, dans lequel l'élastomère contient un groupe fonctionnel dérivé d'un agent de terminaison de polymérisation et dans lequel l'agent de terminaison est l'eau, la vapeur d'eau, un alcool, la 1,3-diméthyl-2-imidazolidinone, un carbodiimide, la N-méthylpyrrolidine, un amide cyclique, une urée cyclique, un isocyanate, une base de Schiff, la 4,4'-bis-(diéthylamino)benzophénone ou un agent répondant à la formule $(R_1)_aZX_b$, dans laquelle Z représente l'étain ou le silicium, R_1 représente un groupe alkyle ayant 1 à 20 atomes de carbone, un groupe cycloalkyle ayant 3 à 20 atomes de carbone, un groupe aryle ayant 6 à 20 atomes de carbone ou un groupe aralkyle ayant 7 à 20 atomes de carbone ; X représente un halogène ou un groupe alkoxy ; a a une valeur de 0 à 3, et b a une valeur de 1 à 4, la somme $a + b$ étant égale à 4.
8. Procédé suivant la revendication 1, dans lequel le mélange comprend du soufre insoluble.
9. Composés élastomère vulcanisés, additionnés d'une charge consistant en silice, pouvant être obtenus par le procédé suivant l'une quelconque des revendications 1 à 8.
10. Bandage pneumatique comprenant un caoutchouc de bande de roulement vulcanisé à partir du composé suivant la revendication 9.